

51 PCT

10/540599

A TWO-COMPONENT WET CEMENT
J620 Reg'd PCT/PTO 24 JUN 2005
PROCESS AND APPLICATION THEREOF

Field of the invention

The present invention relates to a new sialite binary wet cement, and further relates to production method (including package, storage and transportation method) and usage method of the wet cement, and its application.

Prior art of the Invention

For recent 100 years, many novel types of cement, and special cements are appearing ceaselessly. In view of the process technology, Portland cement (also called ordinary cement) is a representative of the traditional modern cements. By means of quite mature knowledge (phase diagrams and phase rules) and technical means, production of Portland cement can be strictly controlled and the product properties can be predicted, because in the final cement clinker of the "one component" cement there are various mineral components having definite compositions and properties. In usage, dry powders of ordinary cement just need to mix with some water, aggregate, (a small amount of regulating agents, water-reducing agent etc. may be added, if necessary), need not to mix with any other activators, and can hydrate themselves to form a concrete. Therefore, the ordinary cement can be called "one component" dry cement.

For recent 50 years, along with rapid increase of the demand of cement and strengthening of human consciousness for harnessing the slag pollution, dust pollution and air pollution, various active or inactive mixed materials are added into Portland cement, and various substitutes of the traditional "one component" cement arise, especially "environment friendly" and cheap cementitious materials are exploited ceaselessly, and they get gradually extensive applications in many fields, in which the Portland slag cement (including Portland fly-ash cement, Portland pozzolana cement) has entered into the main stream of cement industry (see GB1344-1999). For example, by using cinders (pozzolana, fly-ash) to substitute a part of clinker, it forms one type of "mixed material" cement (or called composite cement). In it, the traditional cement clinker still takes a quite big ratio, and the processing concept, route and equipment follow basically those of the existed cement clinkers.

However, when analyzing and understanding new phenomena and rules occurring in the products from hydrating and hardening processes of the composite cement, it is found that the composite cement cannot be clearly explained by the "one component" cement theories.

It is well known that cement is one of three basic materials in the building industry, and has extensive application and great use amounts. Most commonly used cement is Portland cement series, see GB175-1999 (*Portland cement and ordinary Portland cement, Standard No. GB175-1999*). However, the pollution and the damage of environment caused

by the development of cement brings is also a strong enemy of developing civilization of human beings. Cement is generally classified as the following six kinds: Portland cement, ordinary Portland cement, slag Portland cement, fly ash Portland cement, pozzolana Portland cement and composite cement. The later four kinds are classified according to types of the added mixing materials.

All the traditional processes of producing cement include “two milling and one calcining”, i.e., the following three processes: starting material formulating and pulverizing, clinker calcining and cement milling. For the most commonly used Portland cement, the cement clinker is mainly produced from limestone, clay, ferrite powders and coal. The active components in cement clinker are mainly minerals tricalcium silicate and dicalcium silicate, which can form at about 1450 °C or at about 1300 °C with adding some mineralizing agents (see Shen Wei, Huang Wenxi, et. al, *Cement Technology*, Wuhan, Wuhan Industrial University Publishing House, 1990; Yuan Runzhang, *cementitious materials science* Wuhan, Wuhan Industrial University Publishing House, 1996). In producing and using processes of cement, drying, crushing and milling of starting material, calcining clinker and milling cement cause two serious pollutions, namely solid pollution and gas pollution, which also are the “killers” to destroy ecological environment.

Because it is not a abided problem for the human progress that the huge energy, coal, mineral resource, land resource in the cement production are expensed, and that air pollution of harmful gas and dust occur in the milling and calcining processes, especial in calcining clinker, quantity of SO₂, NO_x and CO₂ are discharged to cause serious air pollution, environment pollution, land pollution, water resource pollution and destroy of the ecosystem (See Wu Zhongwei, Tao Yousheng, *present situation and problems of China cement and concrete industries*, fly ash , 1999, (1):3, Wu Zhongwei, *Development Direction of Chinese Cement Industry*, China Building Material, 1999, (4):11).

Today, with rapid development of economy, the industrial waste slag increase continually. The industrial solid waste, such as blast furnace slag and steel slag, nonferrous meal metallurgy slag, power station slag and chemical industry slag, take a rather big ratio in the substance fluid. For example, in China, the total steel output is over 200 million ton per year, and water-quenching slag of blast furnace is about 60 million ton per year, which will be over 100 million ton plus the steel slag. As an example, coal-burning type firepower station is main power station in China. Because of development of the electric industry, number of coal-burning electricity generator increases continually and scale of fire power station increases continually, which results in a rapid increase of fly ash. The total quantity of slag of firepower station in 1985 is 37.68 million ton, and that in 1995 is 99.36 million ton, averagely increasing 5.6 million per year. In 2000, discharge amount of fly ash is 160 million ton, and accumulation of fly ash from power station reaches to 1.2 billion ton, which occupies over 400 thousand mu of land. It is very important how to get a good comprehensive

utilization of the slag. Besides, oil resource of China is relatively meager. In advance, oil importation amount will reach 160 million ton in 2010. It is the national policy to make liquid fuel using coal to substitute for part of oil. It needs 5 ton coal for synthesizing 1 ton oil, if the two-step method is employed (first gasification, then liquefaction). There would give birth of 100 million ton solid slag if 100 million ton oil were synthesized per year (See Jiang Xuerong, Lin Jiedong, et. al., *status of coal-ash comprehensive utilization and its development trend*, electric power environment protection, 2002, 18(3):55; Liu Shuangshuang, Han Mingfang, *present situation and development trend of utilization of fly ash In China*, China Coal, 2001, 27(8):43; Zhu Guilin, Sun Shusan, et. al, *present situation and development trend of resource utilization of metallurgical slag*, China resource comprehensive utilization, 2002, (3): 29; T. Takahashi, K. Yabuta. *New Application for Iron and Steelmaking Slag*. NKK Technical Review, 2002, (87) : 38).

If all the solid waste slag stated above is used, it will be the important technology revolution in energy fields, environment and material fields in 21 century.

The so-called composite materials of cement refer to synthetic and natural mineral materials which are added into cement in order to improve cement properties and to adjust cement grades. In the prior art, the industrial waste slag etc. used in the composite cements as composite material replace a part of cement clinker merely, and cement clinker still constitutes considerable proportions of the cement, and thus it is the main part for imparting cement strength. All the hydraulic cementing fiber slag Portland cements are produced by levigating Portland clinker and granulate blast furnace slag, together with appropriate amount of gypsum. In the cement, blending amount of the granulate blast furnace slag is 20-70% by weight based on total weight of the cement. It is allowable to use one out of limestone, kiln ash, fly ash and pozzolana composite material to replace the slag, but the replace amount cannot exceed 8% by weight of the cement, and in the obtained cement the blast furnace slag is not less than 20%. Pozzolana Portland cement is a hydraulic cementing material produced by levigating Portland clinker and pozzolana mixture together with appropriate amount of gypsum. In the cement, blending amount of the pozzolana mixture is 20-50% by weight based on total weight of the cement. Fly ash Portland cement is a hydraulic cementing material produced by levigating Portland clinker and fly ash together with gypsum, in the cement, blending amount of fly ash is 20-40% by weight based on total weight of the cement. All the hydraulic cementing materials produced by levigating Portland cement, two or more specified composite materials together with appropriate amount of gypsum. Total blending amounts of the composite material is greater than 15% by weight and not greater than 50% by weight based on total weight of the cement. It is allowable to use kiln ash of 8% by weight to replace a part of the composite material, but when slag is blended, blending amount of the composite materials cannot be repeated with the amount of the slag Portland cement (see *Portland cement and ordinary Portland cement standard*, Standard No. GB175-1999;

Portland blast furnace-slag cement, *Portland pozzolana cement and Portland fly-ash cement standard*, Standard No. GB1344-1999; *composite Portland cement standard*, Standard No. GB12958-1999).

More particularly, the composite materials are generally classified as active composite material and inactive composite material. The active composite material is ground to fine powder, and mixed together with lime or gypsum, when water is added thereto, at a normal temperature, hydration products having cementing properties can be formed. The hydration products can be hardened both in water and in air. Inactive composite material doesn't have chemical reaction with the cement components or have merely very weak reaction with the cement components, and therefore the inactive composite substance blended into Portland clinker merely has the following functions: increasing cement output quantity or decreasing cement grade, reducing hydration heat etc. (see Hunan University et al edited, *building materials*, Beijing, China building industry publishing house, 1997).

According to the characteristics of the sialite binary wet cement in the present invention, it can be thought that:

(1) The process of concreting substance of ancient China (such as tabia) has the most original bud of the “binarization”, the air hardening product (it is manufactured by mixing the calcium carbonate treated at high temperature treatment and clay treated not at high temperature) which is used in civil usage in early period and the later period, as well as the hydro-hardening product (it was produced by mixing the clay and calcium carbonate calcined respectively, rice water which functions as plasticizer, and water-reducing agent, and some plant fiber which function actually as a reinforced material) used in tombs of kings and emperors, tombs of patricians, the Great Wall, bastion and castles.

(2) The cementitious materials (according to Davidovite, it is called clay aggregating cement) used in pyramids of ancient Egypt were obtained by the process that the calcined clay and other starting materials conducted “secondary (net-work) feldsparization” at room temperature, and these also have a bud of the characteristics of the “binarization” process.

(3) The cementitious material (pozzolana containing calcium,) of the ancient Roman is a transition representative from the most original “binarization” process to “one component” process.

It can be seen that the development history of cementitious materials undergoes a negation by a negation track which is progressing in a screw form.

Why has not the original binary system developed? The possible reasons are as follows:

- (1) The theory of “one component” process has studied quite perfectly;
- (2) The “one component” cement products have occupied the regnant position absolutely.
- (3) Mind of people has got into the formulary of “one component” cement, and

limited by “one component” process consciously or non-consciously and cannot jump out of it.

Therefore, we look forward imminently to opening up a new approach of the cement industry. Firstly, it is necessary to breach the theoretical bondage of the current “one-element” cement, and to achieve breakthroughs in production process, starting material selection, product storage, and transportation and usage method. Furthermore, it is expected to use the great number of industrial waste residue, fly ash, and the disposal resources from industry, building, traffic, water conservancy, thereby solving the problems of the industrial waste slag occupying land and causing pollution.

Summary of the Invention

First object of the present invention is to provide a new cementitious material called sialite binary wet cement. It is composed of the “female body” as a primary component and the “male body” as a secondary component. The “female body” of the sialite binary wet cement is always in a wet form mixed with water during the whole period of its production, storage, transportation and usage; the secondary component of the wet cement can exist in wet form or dry powder form. The “female body” and the “male body” are produced, stored and transported separately. When the “female body” and the “male body” are used, they just are mixed together.

Second object of the present invention is to provide a new process for producing the sialite binary wet cement, which mainly uses a wet-milling process, and almost no dust occurs during whole producing processes.

Third object of the present invention is to provide starting materials for producing the “female body” of the sialite binary wet cement, which mainly use the mass materials having amorphous and/or microcrystal structure, such as various water-quenching mineral slag, as primary component, together with some regulating agent having conditioning effects and pozzolana active mixture materials.

Fourth object of the present invention is to provide a series of active mixture materials, which includes active mixture materials from both solid industrial slag and natural active materials.

Fifth object of the present invention is to provide a method for producing starting material of the “female body” of the sialite binary wet cement.

Sixth object of the present invention is to provide a method for using the sialite binary wet cement.

Seventh object of the present invention is to solve the existing problem that industrial slags occupy land and produce big pollution sources, due to the fact a great deal of industrial slag was used during producing process of the sialite binary wet cement. In comparison with the industrial waste slag etc. used in the composite cements of the prior art, the sialite binary

wet cement of the present invention has an important difference, namely when the used industrial waste slag have completely same chemical compositions, the composite cement according to the prior art replace a part of cement clinker merely, and the cement clinker still constitutes considerable proportions of the cement, and thus the cement clinker is the main part for imparting cement strength, in contrast, in the sialite binary wet cement of the present invention the industrial waste slag is the main part for imparting cement strength.

The sialite binary wet cement is entirely different from the traditional cement--the ordinary “one component” dry cement. It is a new type of cementitious material, called binary cement, which primary component is a slurry, paste or wet powder composed of fine inorganic cementitious materials together with a small amount of regulating agents and water. The fine inorganic cementitious materials have a fineness degree which results in a specific surface area of 2800-7500cm²/g (see the Standard: *Test method for fineness of cement* (GB1345-91)). The sialite binary wet cement is mainly composed of the “female body” (primary component) and the “male body” (secondary component). The primary component exists always in a wet form, and thus avoids causing dust, in whole manufacturing, storing, transporting and using processes. Its secondary component can exist in a wet form or a dry powder form. The “female body” and the “male body” must be produced, stored and transported separately, and cannot be mixed together before they are used. The “female body” slurry and “male body” slurry do not solidify when stored separately. When adding the “male body” into the “female body”, the “male body” excites the activity of the “female body” and in the meantime will take part in reactions, interactions and accordingly cause chemical reaction (including liquid phase reaction, solid phase reaction) so as to form concreting product (including crystal type, concreting type, net-work type or their mixture), and finally form a sialite having very high strength.

The naming basis for the sialite binary wet cement of the present invention:

(1) For the traditional cements in the prior art, the process technology is same (i.e. “one component” method). As for naming of the cements, they are named by their main starting materials, such as Portland cement, aluminous cement, sulphoaluminate cement and so on. The traditional cements are characterized in that they are always in a dry form in the whole processes from manufacture, storage, transportation up to before usage, and their hydrating product is a type of hydrating silicate with high-calcium.

(2) In modern cement industry, composite cements take quite big ratio, and also use the naming principle according to their main components, such as silicate mineral slag (pozzolana, fly ash) cement etc.

(3) The sialite binary wet cement of the present invention is comprised of two components--“female body” and “male body” both of which are obtained by a series of starting materials. The binary wet cements are characterized by they are always in a wet form in the whole processes from manufacture, storage, transportation up to before usage, and thus

the cements are clean, and have no pollution, and their product is “stone”, which is different from the artifact-- hydrating silicate with high-calcium, which is obtained by the traditional “one component” dry cement.

According to the first aspect of the present invention, there is provided a sialite binary wet cement, characterized by that it is composed of a “female body” (as a primary component) and a “male body” (as a secondary component) both of which are produced, stored, and transported separately, and are mixed together when they are used, wherein the “female body” and the “male body” each have a specific surface area of 2800-7500 cm²/g, the “female body” is mainly composed of inorganic cementitious materials and water, and it is slurry, paste or wet powder form during the whole period of its production, storage, transportation and usage; the “male body” is mainly composed of inorganic cementitious materials, and it can be a wet form or a dry powder form during the whole period of its production, storage, transportation and usage;

proportion of the two components of the wet cement is that the “female body” ranges from 20% by weight to 99% by weight, the “male body” ranges from 1% by weight to 80% by weight; preferably, the “female body” ranges from 60% by weight to 99% by weight, and the “male body” ranges from 1% by weight to 40% by weight; more preferably, the “female body” ranges from 70% by weight to 95% by weight, and the “male body” ranges from 5% by weight to 30% by weight;

in the “female body”, as proportion of its main constituents, CaO ranges from 1% by weight to 60% by weight, Al₂O₃ ranges from 1% by weight to 60% by weight, SiO₂ ranges from 2% by weight to 70% by weight, MgO ranges from 0 % by weight to 40% by weight, and Fe₂O₃ ranges from 0% by weight to 25% by weight; preferably, CaO ranges from 20% by weight to 55% by weight, Al₂O₃ ranges from 2% by weight to 25% by weight, SiO₂ ranges from 20% by weight to 50% by weight, MgO ranges from 4 % by weight to 13% by weight, and Fe₂O₃ ranges from 0% by weight to 12% by weight; and

in the “male body”, pH=7-14, and as proportion of its main constituents, CaO ranges from 0% by weight to 80% by weight, SO₃ ranges from 0% by weight to 55% by weight, and R₂O ranges from 0% by weight to 80% by weight; preferably, CaO ranges from 0% by weight to 40% by weight, SO₃ ranges from 0% by weight to 40% by weight, and R₂O ranges from 0% by weight to 20% by weight, and at least one of CaO, SO₃ and R₂O is greater than 0% by weight, and wherein R is an alkali metal such as K, Na.

The “female body” of the sialite binary wet cement further comprises a regulating agent which is added during production period or/and after production of the “female body”.

The “female body” is a wet material produced by wet-milling one or more selected from amorphous or/and microcrystal iron-making slag, steel-making slag, blast furnace slag, fly ash, waste glass, phosphorus slag, titanium slag, fluorite slag, burned coal fine slags, and their mixtures, as well as water and a regulating agent.

On one hand, the “female body” of the sialite binary wet cement is a wet material which may be obtained by mixing the amorphous or/and micro-crystal coal-burning boiler slag together with water and a regulating agent, and then wet-milling them. Such method comprises the following steps: various amorphous or/and micro-crystal metallurgical slags and coal-burning boiler slags, for example, boiler slags from various industrial boilers which take coal (including the fine coal, slurry coal, lump coal) as its fuel and may include the boilers from thermal power plants, blast furnace and fluidized-bed, coal chemical industry (including coal gasification, coal liquefaction),

adding a given amount of calcium-rich substance (including quick lime, slaked lime and lime stone) and a small amount of mineralizing agents (such as iron powders, calcium fluoride) into the fuel fine coal, slurry coal or lump coal,

melting the burned fine coal slags at high temperature during deslagging process or during the treatment process following after the deslagging step so as to melt partially or entirely the slag, and

then carrying out a rapidly cooling step (such as wind cooling or water-quenching cooling), and thereby obtaining the amorphous or/and micro-crystal materials as the starting materials of the sialite binary wet cement. In this regard, the expectant amorphous and microcrystal product may be obtained with not increasing or a little increasing coal consumption amounts of boiler or with use of the remaining heat, and at the same time an additional benefit for consolidating sulfur in the burning coal and for removing SO₂ in the boiler flue gas.

More particularly, the coal-burning boiler slag is from various industrial boilers which take coal (including the fine coal, slurry coal, lump coal) as its fuel and may include the boilers from thermal power plants, blast furnace and fluidized-bed, coal chemical industry (including coal gasification, coal liquefaction). A given amount of calcium-rich substance (including quick lime, slaked lime and lime stone) and a small amount of mineralizing agents (such as iron powders, calcium fluoride) were added into the fine coal, slurry coal or lump coal (called “adding calcium in the fuel” method); during deslagging process (when the slag is inside hearth or is departing from hearth) or during the treatment process following after the deslagging step, a high-temperature melting step is carried out so that the slags were melted partially or entirely. Then a rapidly cooling step (such as wind cooling or water-quenching cooling) was carried out, and thereby to obtain the amorphous or/and micro-crystal materials.

Or alternatively, a given amount of calcium-rich substance (including quick lime, slaked lime and lime stone) and a small amount of mineralizing agents (such as iron powders, calcium fluoride) into the coal ash and slag (called “adding calcium in the slag” method). During deslagging process (when the slag is inside hearth or is departing from hearth) or during the treatment process following after the deslagging step, a high-temperature melting

step is carried out so that the slags were melted partially or entirely. Then a rapidly cooling step (such as wind cooling or water-quenching cooling) was carried out, and thereby to obtain the amorphous or/and micro-crystal materials.

On other hand, the “female body” of the sialite binary wet cement may be a wet material produced by taking the amorphous or/and microcrystal glass substance located in the zone between Portland cement and glass in the CaO-Al₂O₃-SiO₂ ternary phase diagram (see Figure 4) as starting material, and obtaining a microcrystal and/or vitreous substance having potential water-hardening activity through the steps of starting materials selecting, formulating, mix-milling, calcining and melting, then mixing the obtained substance together with water and regulating agents, and carrying out a wet-milling step

The “female body” of the sialite binary wet cement may be a wet material produced by mixing natural minerals (one of shale, clay, coal gangue or their mixture) calcined and dewatered at 500-1000°C, together with water and regulating agents, then carrying out a wet-milling step.

The “female body” of the sialite binary wet cement may be a wet material produced by mixing the calcined products taking clay (one or more selected from waste bricks, waste tiles and waste ceramics, and their mixtures) as a main component, together with water and regulating agents, then carrying out a wet-milling step to form a wet material.

Furthermore, the inorganic cementitious material of the “female body” may be one or more selected from pozzolana, perlite, obsidian, pumice, sand stone, quartz sand, mine tailing, zeolite, silica fume and their mixtures.

The “male body” of the sialite binary wet cement is produced by mixing one or more selected from natural anhydrite, dihydrate gypsum, hemihydrate gypsum, chemical industry gypsum (such as phosphogypsum, fluorgypsum, salt gypsum), lime, calcium hydroxide, chemical industry lime, strong alkali, strong alkali salt, cement clinker and their mixtures, together with water and a regulating agent, and then carrying out a wet-milling step.

Or alternatively, the “male body” of the sialite binary wet cement is produced by mixing one or more selected from natural anhydrite, dihydrate gypsum, hemihydrate gypsum, chemical industry gypsum (such as phosphogypsum, fluorgypsum, salt gypsum), lime, calcium hydroxide, chemical industry lime, strong alkali, strong alkali salt, cement clinker and their mixtures, together with a regulating agent, and then carrying out a dry-milling step.

In the sialite binary wet cement, the regulating agent for regulating solidifying time of the “male body” and “female body” (see, *test methods for water requirement for normal consistency, setting time and soundness of the Portland cements* (GB1346-89)) is made of one or more selected from sugars, honeys, citric acid and citrate, tartaric acid and tartrate, strong alkali, dissolvable carbonate, muriate, dissolvable silicate, dissolvable sulfate, water glass, chlorinate, lignosulphonate, boric acid, borate and their mixtures.

In the “female body” of the sialite binary wet cement, water content is 0.1%-95% by

weight, preferably 10%-80% by weight, more preferably 25%-70% by weight.

In the “male body” of the sialite binary wet cement, water content is 0%-95% by weight, preferably 15%-85% by weight, more preferably 25%-70% by weight.

A method for producing the sialite binary wet cement is as follows: under the premise of satisfying a required specific surface area, using different combinations of machines suitable to wet-crushing and wet-milling, and using a method called “mixing first, then milling” in which starting materials of the “female body” and starting materials of the “male body” are mixed first in their own proportions respectively, and then they are wet-crushed and wet-milled. Or alternatively, using a method called “milling first, then mixing” in which starting materials of the “female body” and “male body” are wet-crushed and wet-milled first respectively according to grindability, then mixing and homogenizing the levigated starting material in their own proportions so as to obtain a wet material respectively. The obtained wet materials for the “female body” and “male body” should be stored and transported separately.

The “male body” of the sialite binary wet cement may comprise further a regulating agent which is added during production period or/and after production of the “male body”.

If a regulating agent is added when the “female body” of the sialite binary wet cement is produced, and it is preferable that fineness degree of the regulating agents is chosen so that specific surface area is (4000-5000) cm²/g.

During production, storage, transportation and use of the sialite binary wet cement, the regulating agent may be added in amount of from greater than 0% to 10%, preferably from greater than 0% to 5% by weight based on the total weight of the “female body” and “male body” of the sialite binary wet cement.

During production package, transportation, storage and/or usage period, the “female body” and “male body” of the sialite binary wet cement, a watering or dewatering apparatus may be used.

A method for using the sialite binary wet cement may comprise merely mixing the “female body” and “male body” in proportion, and if necessary, water may be added to cause a hydrating reaction and a chemical reaction between liquid phase and solid phase, thereby forming cementitious materials which is one of crystal type, gel type, network type or their mixtures. Because the sialite binary wet cement has a hydration mechanism different from that of “one component” cement such as Portland cement, and it has good consolidation ability to a granule-rich grade aggregate (for example clay, sludge, mine overflow tailing), it is used to replace the traditional Portland cement (“one-component” dry cement), and used in various engineering constructions, such as building, traffic, water conservancy, mine backfill and timbering, subgrade strengthening or underground engineering, and used for consolidating clay, sludge, sand soil, fly ash, metal ore dressing tailings and for cementing and filling the mine, wall material or other field, thereby the binary wet cement has more wide usage and application field in comparison with the traditional cement.

As one method for producing the sialite binary wet cement according to claim 1, under the premise of satisfying a required specific surface area, using different combinations of machines suitable to wet-crushing and wet-milling, and using a method called “mixing first, then milling” in which starting materials of the “female body” and starting materials of the “male body” are mixed first in their own proportions respectively and then they are wet-crushed and wet-milled so as to obtain a wet material respectively; and storing and transporting separately the obtained wet materials for the “female body” and “male body”.

As other method for producing the sialite binary wet cement according to claim 1, under the premise of satisfying a required specific surface area, using different combinations of machines suitable to wet-crushing and wet-milling, and using a method called “milling first, then mixing” in which starting materials of the “female body” and “male body” are wet-crushed and wet-milled first respectively according to grindability, then mixing and homogenizing the levigated starting material in their own proportions so as to obtain a wet material respectively; and storing and transporting separately the obtained wet materials for the “female body” and “male body”.

When the sialite binary wet cement is used in manufacturing concrete, the “female body” and “male body” of the wet cement are mixed and agitated together with water and an aggregate to manufacture concrete. The aggregate may be selected from one or more of mountain sand, river sand, sea sand, gobi sand, crushed stone, bulk stone, waste stone, coal gangue, clay, mineral classified sand, whole mineral tailings, industrial waste slag and their mixtures.

It can be seen that, from the comparison of the sialite binary wet cement and common ordinary Portland cement, it can be seen that the wet cement of the present invention is innovative no matter from the view of the source of starting material, processing, management, hydrate and hardening mechanism, usage and properties of production, and has more extensive application than the traditional cement.

The first prominent advantage of the sialite binary wet cement in the present invention is that: it breaks restrictions and limits of the process of traditional cement, and provide a new wet process for producing cement, and establishes the basis to entirely solve the environment pollution of cement industry. The process flowchart can be seen in Figure 1, Figure 2, Figure 3, Figure 5, and Figure 6 (the details are shown in the figures). The dust pollution are greatly reduced or even wholly eliminated in the producing process of the sialite binary wet cement. The wet-crushing and wet-milling process can radically avoid the dust pollution, which cannot avoid in the traditional dry process. So SO₂, NO_x and CO₂ are reduced greatly or even eliminated entirely, not causing pollution to environment.

The second prominent advantage of the present invention is that 95% to 100% of starting materials for producing the sialite binary wet cement need not be calcined, and this is equal to save the expenses for constructing, running, managing, material and energy

consumption for the clinker production part of the same scale cement factory. Furthermore, all the starting materials need not dry-treated. Their storage, piling up and transportation doesn't need special maintenance. The starting materials entering the factory are wet-crushed and wet-milled directly, which is not only saving energy, but also saving time, saving work, simplifying production process greatly, and accordingly the production and management costs are reduced greatly.

The third prominent advantage of the present invention is that noise is much less comparing to that of the traditional dry-milling equipment; and the milling efficiency increases. For example, in Example 1, in the case for obtaining the same fineness degree (specific surface area), the output can increase greatly; in Example 2, in the case for obtaining the same output, the fineness degree (specific surface area) can increase greatly.

The fourth prominent advantage of the present invention is that the sialite binary wet cement can reduce greatly consumption and occupation of the land resource in its producing process, and the starting materials of the sialite binary cement is basically entirely the industrial waste, thereby changing waste into treasures and improving the ecotypic environment.

Brief description of the drawing

Figure 1 is a flowchart graph for producing the “female body” of the sialite binary wet cement.

Figure 2 is a flowchart graph for producing the “male body” of the sialite binary wet cement.

Figure 3 is a flowchart graph for producing the “male body” of the sialite binary wet cement by dry-milling method.

Figure 4 is a ternary phase diagram for CaO-Al₂O₃-SiO₂ system.

Figure 5 is a graph showing production process for producing the “female body” of the sialite binary wet cement.

Figure 6 is a graph showing production process for producing the “male body” of the sialite binary wet cement.

Detailed description of the preferred embodiments

(A) Inventive concept of the sialite binary wet cement according to the present invention

(1) The sialite binary wet cement is composed of two components-- “female body” and “male body”, and the primary component is in wet form, different from the “one component” cement, which is mainly composed of the cement clinker and must be in dry powder form. In the sialite binary wet cement of the present invention, industrial waste slag is the main components for providing strengths.

In the traditional composite cements, relevant composite materials are added to the composite cements for playing merely a role of second hydration, and are not major elements of hydration. This is an essential difference between the traditional composite cements and the binary wet cement. The binary wet cement uses solid waste slag as main body of the cementitious materials. Use amount of the solid waste slag can be continuously adjusted within a great scope according to working operation requirements, environments, processes and so on. Since quantitative change of the addition amount of the solid waste slag will cause a qualitative change, which is manifested by that the hydration product is different from that of the traditional cements, its physical properties change, especially the mechanical properties change, for example, it has high strength, high compactness and high durability. At present, in most cases, usage of solid waste slag has low value-added contents, and doesn't exert activity of the solid waste slag. There are a few of usage method which can bring out innoxiousness and impart high value-added contents. The binary wet cement use mechanical-chemical method, chemical activating method and lithifying method etc. to exert activity of the solid waste slag.

Because properties of the binary wet cement is greater than or near to properties of Portland cement, in the present invention the binary wet cement is compared with Portland cement.

(2) The two components -- “female body” and “male body” in the sialite binary wet cement have different history (heat history and stress history) respectively. They can be stored and transported respectively for long time and do not agglomerate.

(3) The sialite binary wet cement is obtained by that the “female body” and “male body” hydrate, interact each other and react chemically (including liquid phase reaction and solid phase reaction) at a room temperature.

(4) In view of the weight ratio of quantity, and in view of the substance source of the reaction products, the “female body” is the substance that has better potential reaction activity and is the primary component of cementitious material.

(5) The “male body” is the secondary component that can make the “female body” to produce activity, though its content can be less than that of “female body”. Its effects include:

(i) Exciting activity of the “female body” and providing necessary reacting conditions (such as pH);

(ii) Co-reacting with the “female body” and constituting the concreting product as a part of reactant (crystalline type, gel type, net type or their mixture).

Through experiment, study, analysis to the binarization processes of the present invention, it is determined that the above four problems are solved partially by using industrial waste slag (including and various amorphous and microcrystal solid waste slag), which does not cause air pollution in producing process and has a certain activity, as starting materials, the following three problems must be solved:

1. Determining components and compositions of the binary wet cement;
2. Making the binary wet cement not to solidify for a long period (several hours to several years);
3. Making the binary wet cement to be able to solidify at its normal condition and have very high strength.

(B) "Female body" and "male body"

The "female body" and "male body" can be divided into two types:

(1) The "female body" has reaction activity itself, and the chemical reaction can spontaneously conduct under a certain condition to form cementitious substance; and function of the "male body" is to supply the reaction condition, and excite reaction activity of the "female body" and make the reaction activity exert adequately and result in good strength.

(2) The "female body" has certain reaction activity itself, and can react with the "male body" under certain condition to form concreting substance. The effect of the "male body" is not only supplying the necessary reacting substance with "female body", but also supplying the reacting condition to make the effect of "female body" exert adequately and result in good strength.

The "female body" and "male body" of the sialite binary wet cement of the present invention have very slow hydration before they are mixed together, and thus they can be stored for a long period without debase of quality. In contrast, the traditional Portland cement is apt to agglomerate, and thus to reduce or loss its cementing capacity, and as a result, its strength is reduced significantly. Even if under a good storage condition, the traditional cement cannot store for a long time, since the cement will absorb moisture and carbon dioxide from air, and accordingly retard hydration and cause carbonization, thereby its cementing capacity is lost and strength was reduced largely. Under a general storage condition, after stored for three months, the cement strength reduces by about 10%-20%; after stored for three months, the cement strength reduces by about 15%-30%; and after stored for three months, the cement strength reduces by about 25%-40%.

The "female body" is a main part of the wet cement components. When the manufacture process is carried out in water phase, a storage step is propitious to accelerate a early hydration of the "female body" of the wet cement, and thus a supersaturated reactant concentration is formed, thereby the materials are hydrated and homogenized sufficiently, and accordingly reaction products are formed quickly, and it is possible to improve products quality and to keep consistency of the product quality.

In order to ensure quality of the wet cement, a regulating agent can be added for adjusting spontaneous reaction degree of the "female body". In order to ensure further quality of the wet cement, a regulating agent can also be added for adjusting spontaneous reaction

degree of the “male body”.

One of the important aims of the “female body” of the sialite binary cement is to solve the problem of effective usage and pollution of industrial waste slag, to produce slurry by using one of the industrial waste slag, such as amorphous or/and microcrystal mineral slag including metallurgical slag, such as water-quenching slag, blaster furnace slag, phosphorus mineral slag, titanium slag, fluorite mineral slag, steel making slag, blast furnace slag, various slag of boilers burning coal, fly ash, waste glass, or the their mixtures, adding water and regulating agents, and wet-milling; or to produce slurry by using one of natural mineral calcined and dewatered at 500-1000 °C such as shale, clay, coal gangue, or the their mixtures, adding water and regulating agents, and wet-milling. Another aim is to solve the problem of pollution and effective usage of building garbage so as to produce a slurry by using one of the factory waste products mainly composed of clay and calcined at certain temperature such as waste bricks, waste tiles, waste ceramics or their mixtures, adding water and regulating agents and wet-milling. Another aim is to solve the problem of pollution and effective usage of fly ash so as to produce wet material by using amorphous and/or microcrystal slag of boilers burning coal, i.e., using the coal slag coming from the industrial boilers and thermal power plants using fine coal or slurry coal or bulk coal as their fuel, adding some calcium-rich substance (including quick lime, slaked lime and limestone) and a small amount of mineralizing agents such as iron powders, calcium fluoride into fine coal or slurry coal or bulk, then rapidly cooling (such as wind cooling or water-quenching cooling) the burned slag when the slag departing hearth or being melted to obtain amorphous or/and microcrystal materials, then mixing the materials together with water and regulating agents, and wet-milling process; or to produce a slurry by using amorphous and/or microcrystal slag of boiler burning coal, i.e., using the coal slag coming from the process of coal gasification and converting coal into oil, adding some calcium-rich substance (including quick lime, slaked lime and limestone) a small amount of mineralizing agents such as iron powders, calcium fluoride into fine coal or slurry coal or bulk coal, when the slag departing the hearth or after being melted, rapidly cooling (such wind cooling or water-quenching cooling) the burned slag to obtain amorphous or/and microcrystal materials, then mixing the materials together with water and regulating agents and wet-milling process. The regulating agents can be added in producing process as required, or/and added after producing process as required.

The “male body” of the sialite binary wet cement can be obtained by using one or more of the natural anhydrite or/and dihydrate gypsum, hemihydrate gypsum, chemical industry gypsum (such as phosphogypsum, fluorgypsum, salt gypsum), lime, calcium hydroxide, chemical industry lime, strong alkali and strong alkali salt, cement clinker, various cement or their mixtures, together with regulating agents, and carrying out dry-milling or wet-milling.

The regulating agents of the sialite binary wet cement in the present invention can use

one or more of sugars, honeys, citric acid and citrate, tartaric acid and tartrate, strong alkali, dissolvable carbonate, muriate, dissolvable silicate, dissolvable sulfate, chlorate, water glass, lignosulphonate, boric acid, borate or their mixtures.

The starting material of the “female body” of the sialite binary wet cement can be partially substituted by using one or of pozzolana materials, perlite, pitchstone, obsidian, pumice, shale, coal gangue, limestone, sand stone, quartz sand, clay, natural zeolite, various mineral mine tailing, silica fume or their mixture.

Today, with rapid development of economy, industrial waste slag increase continually. The industrial solid wastes, such as blast furnace slag and steel slag, nonferrous meal metallurgy slag, power station slag and chemical industry slag, take a rather big ratio in the materials circulation. The inventors have studied intensively and extensively the physical and chemical properties of the above solid wastes. For example, the chemical components of fly ash and coal slag in China are silicon dioxide, aluminium oxide, iron sesquioxide, calcium oxide and unburnt-out carbon. At various areas in China and abroad, the composition of the fly ash, coal slag, which are produced by the boilers burning coal, thermal power plants, blast furnace, fluidized-bed, coal chemical industry (including coal gasification, coal liquefaction) are basically similar, and content scopes are generally as follows:

CaO	Al ₂ O ₃	SiO ₂	Fe ₂ O ₃
1-11%	15-40%	30-65%	1-20%

The inventors found that these solid slags have similar main compositions (calculating according oxides) in relative to the cement clinker or the mineral slag having good water-hardening ability, as shown in Table 1:

Table 1

Substance name	Chemical composition (%)				
	CaO	Al ₂ O ₃	SiO ₂	Fe ₂ O ₃	MgO
fly ash	1-11	15-40	30-65	1-20	0.5-2
slag	38-46	7-20	26-42	0.2-2	4-13
Portland clinker	62-67	4-7	20-24	2.5-6	<5

From Table 1, it can be seen that though the three materials contain same types of main oxides, contents are quite different. The main difference is content of the calcium oxide in fly ash and slag is lower than that in mineral slag, and is much lower than that in clinker of Portland cement. This low calcium content is the main reason that the fly ash and coal slag cannot be used as main components of the traditional “one component” cement, and merely be minor components.

The inventors further found that, various water-quenching metallurgical slag have relatively high contents of CaO, SiO₂ and Al₂O₃ (see chemical compositions of slag shown in Table 1), and this kind of the lag is essentially amorphous and microcrystal vitreous materials.

These slags each are melting slag body formed under high-temperature metallurgical condition through water-quenching cooling treatment. For example, when temperature of molten slag is in range of 1400°C to 1700°C, the formed water-quenching ironmaking slag is essentially vitreous materials. This kind of water-quenching metallurgical slag has very high potential hydraulic set activity.

The inventors found further that the silicon oxide, aluminum oxide in coal exists in form of mineral Kaoline ($\text{Al}_4[\text{Si}_4\text{O}_{10}] (\text{OH})_8$). In light of the above characteristics, the inventors found that if according to fly-ash content of coal and required content of calcium oxide in the mineral slag or Portland cement clinker, by adding a certain content of calcium-rich substance (including quick lime, slaked lime, limestone or coal gangue) into the fuel (including fine coal, slurry coal, lump coal) during coal converting process, after mixture of coal is burnt out, it can make the chemical composition, mainly calcium oxide content, of the slag to become the intended chemical compositions of mineral slag or Portland cement clinker; the inventors also found that calcining temperature of cement clinker is about 1450°C, and if adding a small amount of mineralizing agents (such as iron powder, calcium fluoride), the clinker can be obtained at about 1300°C; however, temperature of high-temperature zone of hearth of coal-burning boiler is generally 1300-1700°C, which can completely satisfy the temperature required by calcining to form mineral slag or Portland cement clinker. When coal mixture burns at high temperature in hearth, the added substance react with mineral Kaoline ($\text{Al}_4[\text{Si}_4\text{O}_{10}] (\text{OH})_8$) in coal so as to they are partially or wholly melted, then are rapidly cooled, so that it is possible to form a great amount of microcrystal or amorphous substance with hydro-hardening activity.

The inventors still found that if the calcium-rich substance (including quick lime, slaked lime and limestone) and a small amount of mineralizing agents (such as iron powder, calcium fluoride) are added into the high temperature fly ash and coal slag before departing slag, (if the temperature cannot meet the demand, they can be re-heated), and when they are partly or wholly melted, then are rapidly cooled, it is also possibl to form a great amount of microcrystal or amorphous substance with hydro-hardening activity.

Based on above knowledge, the inventors have conducted a lot of experiment, for example, two representative types are:

1. According to fly-ash content of coal and the intended content of calcium oxide in mineral slag, a sample was by obtained by adding lime into coal to make the chemical composition, mainly calcium oxide content, of the slag so as to reach the intended chemical composition of the slag after coal was burnt out, then partially melting the residual slag sof the coal, then rapidly cooling (water-quenching) them. Through adjusting the added amount of lime to change the content of calcium oxide, a series of the samples were obtained and were tested. The representative chemical compositions are listed in Table 2, and the corresponding strengths can be seen (Example 26)

Table 2 (on weight percent basis)

Sample No.	SiO ₂	Al ₂ O ₃	CaO	MgO	Fe ₂ O ₃
Sample 1	61.54	12.68	21.51	1.55	1.26
Sample 2	38.75	14.63	36.25	6.65	0.78
Sample 3	28.16	12.45	54.46	2.26	1.55

2. According to chemical composition of fly ash and intended content of calcium oxide in the ash slag, a lime was added into the ash slag discharged out after coal being burnt, so as to make the chemical composition, mainly calcium oxide content, of the fly ash mixture to reach the intended values (namely “adding calcium in the slag” method), then partially melted the mixture of fly ash, then rapidly cooling (water-quenching) them. By changing the added amounts of lime, a series of the samples having different contents of calcium oxide were obtained, and they were tested. The representative chemical compositions are listed in Table 3, and the corresponding strength data are shown in Example 27.

Table 3 (on weight percent basis)

Sample No.	SiO ₂	Al ₂ O ₃	CaO	MgO	Fe ₂ O ₃
Sample 4	62.75	13.63	20.25	2.4	0.78
Sample 5	36.85	15.95	35.97	7.85	1.48
Sample 6	26.16	10.45	55.2	3.26	1.55

3. A great number of experimental studies were made by using directly water-quenched slag and steel slag from metallurgical industry.

According to a great number of experimental studies, the inventors further understood that, the rapid-cooled slag coming from metallurgy industry, firepower industry and chemical industry, are mainly micro-crystal and amorphous vitreous material, because their crystals do not have a chance to grow. These micro-crystal and amorphous glasses have high free energy and many structural defects, and test experimentation demonstrates that they have good potential hydro-hardening ability (see Example 26 and Example 27). Such slage will be main starting materials of the sialite binary wet cement of the present invention. Therefore, the industrial boilers using coal (including coke, fine coal, slurry coal, lump coal) as fuel, such as the boilers of thermal power plants, coal chemical industry (including coal gasification, coal liquefaction), and various industrial boilers, blast furnace, fluidized-bed, are added some calcium-rich substance (including quick lime, slaked lime and lime stone) and a small amount of mineralizing agents (such as iron powders, calcium fluoride) in burning process or before burning process or in the process of departing slag or in the process of departing and treating slag. Through partially or wholly melting the slag by utilizing remaining heat or supplementary reheating, then through the rapidly cooling process (wind cooling or

water-quenching cooling), microcrystal and amorphous substance are obtained. This is one important part of the present invention.

(C) Production process of the sialite binary wet cement

The production process of the sialite binary wet cement is different from that of the traditional cement, and the basic different is that the crushing and milling of the starting materials are conducted in water medium not in air, and the manufacture is finished in wet state (slurry, paste, wet powder). The process is quite flexible, for Example, the starting materials can first be wet-crushed and wet-milled respectively, then mixed and uniformed according the ratio, or can first be put up respectively according the difficult degree of crushing and milling, then wet-crushed and wet-milled, finally put up uniformly to obtain slurry and paste which do not need further dry treatment and are the product. They can be used to manufacture concrete immediately or be packaged in bags for storage, transportation and production for usage.

The process and method of production, transportation and package of the “female body” include:

The starting materials need not be dried, and the starting materials are crushed directly and milled into slurry after being mixed with regulating agents (or not using regulating agents) and water. The proper regulating agent can be added in production process according the need, also can be added after manufacture of slurry, and the slurries need store and transport separately. The milling degree of fineness is rendered a specific surface area of 2800-7500cm²/g; the better degree of fineness is rendered a specific surface area of 4000-5000cm²/g; the storage period can be adjusted from several days to several years. Water content is no restricted in principle, and it can be 0.1-95% by weight, preferebaly 10-80% by weight, mostly prefereably 25-70% by weight. The crushing and milling method of starting materials can be controlled flexibly. The starting materials can wet-crushed and wet-milled respectively first, then be uniformly mixed according the ratio; or the starting materials can first be put up respectively according to their grindability, and then were wet-crushed and wet-milled, and finally were homogenized. In the whole processes, the dewatering equipment or watering equipment can be equipped. After wet-crushed, wet-milled and homogenized, the obtained “slurry, paste, wet powder” materials can be used directly to manufacture concrete, or be packaged, transported and stored for further use. The transportation and package can use bulk cement tank-cars, or various packages forms such as recycle barrel or tank having various sizes, or disposable polymer bags or weaving bags etc.

The process and method of production, transportation and package of the “male body” include following two types:

(1) The starting materials for dry-milling are dried, crushed, and milled with or without usage of regulating agents to form a dry powder. The powder has a fineness which

renders a specific surface area of 2800-7500cm²/g. A preferable fineness is rendered a specific surface area of 4000-5000cm²/g. They should be stored and transported separately. The regulating agents can be added in the manufacturing process as required, or added after the manufacturing process as required.

(2) The starting materials for wet-milling are not dried, then are crushed and milled into wet slurry by adding water and with or without the usage of regulating agents. The slurry has a fineness which is rendered a specific surface area of 2800-7500cm²/g. a preferable fineness is rendered a specific surface area of 4000-5000cm²/g. The regulating agents can be added during the manufacturing process as required, or added after the slurry was produced as required. They are stored and transported separately. In wet-milling form, the storing period can be adjusted from several days to several years. Water content of the “male body” is not restricted in principle, it can be 1-95% by weight, preferebaly 15-85% by weight, mostly prefereably 25-70% by weight. In wet-milling, the process can be controlled flexibly, and the starting materials can be wet-crushed and wet-milled separately, then uniformly mixed in a specific ratio; or the starting materials can first be put up respectively according to their grindability, and then wet-crushed and wet-milled, finally be uniformed. In homogenizing, the dewatering equipment can be equipped. After wet-crushed, wet-milled and homogenized, the obtained “slurry, paste, wet powder” materials can be used directly to manufacture concrete, or be packaged, transported and stored for further use. The transportation and package can use bulk cement tank-cars, or various packages forms such as recycle barrel or tank having various sizes, or disposable polymer bags or weaving bags etc.

The stated regulating agents of the sialite binary wet cement can be added into “female body” or into “male body” or into both of them.

(D) Equipment used for producing the sialite binary wet cement

Under the premise of satisfying the demanded specific surface area, various combination of machines suitable to wet-crushing and wet-milling can be selected, such as the machine combine selected from one, two or three of roll mill, disc mill and ball mill, see Figure 1 and Figure 2. The production scale can be big or small to satisfy the need of the big scale and centralizing production and the small-scale production at several positions and according the needed quantity. If necessary, dewatering equipment or watering equipment can be equipped. If the producing scale is small, the needed cost of producing equipment of the binary wet cement is low, so that it can suit measures to different conditions, and it need not devote a great deal of capital to establish big scale producing entertainment, and that it is benefit to harness the industrial solid waste slag in large-scale.

(E)The using method of the sialite binary wet cement

When being used, the “male body” and “female body” are needed to be mixed to act

each other, and then can cause hydrate reaction and chemical reaction (including liquid phase reaction, solid phase reaction) to form concreting substance (including crystal type, gel type, net-work type or their mixture), and finally to form sialite. The following is to give a relevant examples.

In the usage of building, the sated sialite binary cement can produce concrete by mixing it with aggregate and water and mixing round them, and the method is as same as that of the common concrete. The aggregate to produce concrete is composed by one of the mountain sand, river sand, sea sand, gobi sand, milled sand, crushed rock, bulk rock, waste rock, mine tailing rock, clay, mine classified sand, whole mineral tailings and industrial waste slag or of their mixtures. The produced concrete can be used in building, irrigation works, communication, underground engineering etc.

In the usage of mineral backfill, timbering, separating wind and stopping leak, roadbed reinforcement, the sated sialite binary wet cement has very strong solidifying ability to the sand soil containing high content clay except having the same application like the cement, and is much suitable to be used to mine backfill, timbering, separating wind and stopping leak, roadbed reinforcement and so on. Because cement is used as cementitious material to backfill in mines now, the concreting time is long, the strength of the backfill substance is low, and the backfill cost is high. Because the backfill cost is high, the exploited space of most of the mines do not be backfilled, being let fall down naturally, so that it results in the ground settle, underground water pollution, destroy of the ground constructions and environment, and so much as disaster.

When using traditional cement as cementing material, generally the classified sand mine tailing is used as backfill material. The fine sand (less than $37 \mu\text{m}$) can not be used, and need to be sent to mine tailing storehouse, which increases the difficulty of piling dam and raises constructing expense of mine tailing storeroom. In the mines that has high grade and low mine tailing producing ratio, the backfill aggregate is seriously lack and is recruited using milling sand or bought sand so that the backfill cost increases further. If the sialite binary cement of the present invention is used as backfill material, the mine tailing need not be classified. It can concrete the fine mine tailing sand and fine mud together so that the backfill cost greatly deceases. The method and process are:

- (1) Mixing the sialite binary cement together with water or together with botha water and the added aggregate or together with slurry containing the added aggregate respectively to manufacture a backfill slurry, in which content of the sialite binary cement as concreting agent is 2-15% of that of backfill slurry.
- (2) The backfill slurry is made to a concentration of 35-87% by weight, prefereably 60-85% by weight.
- (3) Sending the manufactured backfill slurry to the backfill position through flowing automatically or by pumping.

(F)Example

In Figure 1, the storehouse No.1 is used to store various water-quenching slag with amorphous or/and microcrystal structure, such as blaster slag, phosphorus mineral slag, titanium mineral slag, manganese mineral slag, fluorite mineral slag; the storehouse No.2 is used to store steel making slag, blast furnace slag, fly ash, waste glass, coal-burning boiler slag or the natural mineral shale calcined and dewatered at the temperature 500-1000°C, clay, coal gangue, or the factory waste products using clay as main component and sintered at certain temperature, such as waste bricks, waste tiles, waste ceramics, or the mixing materials, or pozzolana materials, perlite rock, turpentine rock, obsidian, pumice, shale, coal gangue, limestone, sand stone, quartz stone, clay, natural zeolite, pumice, various mineral mine tailing, silica fume or the amorphous and microcrystal substance that is obtained in boilers and power stations using fine coal as fuel, through adding calcium-rich substance (including quick lime, slaked lime, limestone) and a small amount of mineralizing agents into fine coal, slurry coal or bulk coal, and through wind cooling or water-quenching the burned residual product when or after they are departed the hearth or after they are melted, or the amorphous and microcrystal substance that is obtained in boilers using bulk coal as fuel, blast furnace, fluidized-bed and thermal power plants, through adding calcium-rich substance (including quick lime, slaked lime, limestone) and a small amount of mineralizing agents into bulk coal, and through air wind cooling or water-quenching cooling the burned residual product when they are departed from the hearth or after they are melted, or the amorphous and microcrystal substance that is obtained in the process of manufacturing oil by coal, through adding calcium-rich substance and a small amount of regulating agents into fine coal , slaked coal or bulk coal , and through wind cooling or water-quenching the burned residual product after they are departed from the hearth or melted.

The substances in storehouses No.1 and No. 2 are the main starting material of the “female body”. In substance, they are the substances which have potential hydro-hardening activity and microcrystal or/and amorphous structure, and are obtained through mixing several inorganic materials in certain ratios, milling and calcining them, letting their composition to be between Portland cement and glass in the ternary phase diagram of $\text{CaO}-\text{Al}_2\text{O}_3-\text{SiO}_2$, then melting and rapidly cooling them (wind cooling or water-quenching cooling).

The storehouses No.1 and No. 2 in Figure 2 and Figure 3 are used to store one of the natural anhydrite, dihydrate gypsum, hemihydrate gypsum, chemical industry gypsum (phosphogypsum, fluorgypsum, salt gypsum), lime, calcium hydroxide, chemical industry lime, alkali materials, various cement clinker, various cement or their mixtures, which are the main starting materials of the “male body”.

The process of manufacturing the sialite binary wet cement also includes:

(1) The wet-crushing and wet-milling equipment can be set up at the concrete workstation, which can be done that crushing and milling can be conducted at the moment when they are needed. They need not be stored for long period, and do not cause the problem of grade reduce or failure of the cement, and need not build the rainproof and waterproof construction, and do not need special preservation, saving labor, saving substance, and reducing cost.

(2) The crushing and milling equipment can also be set up near the starting material resource or the work site. It just needs to transport the starting materials or the sialite binary wet cement packaging in bags in short distance, greatly saving substance fluid cost and the occupation of transporting resource.

The following is to describe particularly flowchart graph for producing the sialite binary wet cement.

1. Flowchart graph for producing the “female body” of the sialite binary wet cement is shown in Figure 1.

Storehouse No.1 is used to store the materials having a particle size of less than 20mm, such as water-quenching slag; storehouse No.2 is used to store the materials having a particle size of greater than 20mm, such as coal gangue; storehouse No.3 is used to load a regulating agent; storehouse No.4 (or container) is to load water. The production flowchart comprises the following steps:

(1). According to proportioning requirements, the materials from storehouse No.2 were crushed, then the crushed materials, the starting materials of storehouse No.1, regulating agent of storehouse No.3 and water of storehouse No.4 were weighed respectively, and then letting them to pass through an iron removal apparatus;

(2). Removing iron from the materials by using the iron removal apparatus and then sending the materials into a mill;

(3). Mixing thoroughly and uniformly the materials during water-milling process and milling the materials into a fine slurry, and then sending the slurry to a spiral classifier;

(4) The spiral classifier sent back non-levigated materials out of the slurry to the mill for milling them again, and sent the levigated slurry to watering and dewatering apparatus (which adds water to the slurry or removes water from the slurry according to specific requirement);

(5). The slurry in the watering and dewatering apparatus was added water thereinto or removed water therefrom, and then entered into a warehouse; and

(6). The slurry in the warehouse was weighed and then sent to a ladle car, and left factory without packing. Or alternatively, the slurry may be weighed and then packed before leaving factory.

2. Flowchart graph for producing the “male body” of the sialite binary wet cement is shown in Figure 2.

Storehouse No.1 is used to load the materials having a particle size of greater than 20mm such as gypsum; storehouse No.2 is used to load the materials having a particle size of greater than 20mm such as steel slag; storehouse No.3 is used to load a regulating agent; and storehouse No.4 is used to water. The production flowchart comprises the following steps:

(1). According to proportioning requirements, the materials from storehouse No.1 and storehouse No.2 were crushed, then the crushed materials, regulating agent of storehouse No.3 and water of storehouse No.4 were weighed respectively, and past through an iron removal apparatus;

(2). Removing iron from the materials by using the iron removal apparatus and then sending the materials into a mill;

(3). Mixing thoroughly and uniformly the materials during water-milling process, and milling the materials into a fine slurry, and then sending the slurry to a spiral classifier;

(4) The spiral classifier sent back non-levigated materials out of the slurry to the mill for milling them again, and sent the levigated slurry to watering and dewatering apparatus (which adds water to the slurry or removes water from the slurry according to specific requirement);

(5). The slurry in the watering and dewatering apparatus was added water thereinto and removed therefrom, and then entered into a warehouse; and

(6). The slurry in the warehouse was weighed and then sent to a ladle car, and left factory without packing. Or alternatively, the slurry may be weighed and then packed before leaving factory.

3. Flowchart graph for producing the “male body” of the sialite binary wet cement by dry-milling manner is shown in Figure 3.

Storehouse No.1 is used to load the materials having a particle size of greater than 20mm, such as steel slag; storehouse No.2 is used to load the materials having a particle size of greater than 20mm, such as coal gangue; storehouse No.3 is used to load grinding aids; storehouse No.4 used to load the materials having a particle size of less than 20mm. The production flowchart comprises the following steps:

(1). According to proportioning requirements, the materials from storehouse No.1 and storehouse No.2 were crushed, then the crushed materials, regulating agent of storehouse No.3 and materials of storehouse No.4 were weighed respectively, and past through an iron removal apparatus.

(2). Removing iron from the materials by using the iron removal apparatus, and then sending the materials into a mill.

(3). Mixing thoroughly and uniformly the materials during dry-milling process, and milling the materials into a fine powder, and then sending the powder to a powder concentrator.

(4) The powder concentrator sent back non-levigated materials out of the powder to the mill for milling them again, and sent the levigated materials to a warehouse.

(5). The material in the warehouse was weighed, and then sent to a ladle car, and left factory without packing. Or alternatively, the slurry may be weighed and then packed before leaving factory.

Examples of production processes of the sialite binary wet cement

1. Flowchart graph for producing the “female body” of the sialite binary wet cement is shown in Figure 5.

Production technique for producing the sialite binary wet cement comprises: starting material storage area 1, clampshell crane 2, hammer crusher 3, bucket elevator 4, belt conveyer 5, charge distributor and belt weigher 6, starting material storehouse 7, ball mill 8, spiral classifier 9, enriching machine 10, ceramic filter 11, finished product package line 12, bulk finished product package line 13. The production flowchart comprises the following steps:

(1) Clampshell crane sent the various starting materials respectively from the starting material storage areas to corresponding storehouses for backup.

(2) Storehouses used charge distributors and belt weighers to formulate a mixture in a specific proportion, and belt conveyer sent the mixture to a first-stage mill, and at the same time a given amount of water was supplied to the mill by a pipeline.

(3) The slurry material discharged from the first-stage mill was sent directly to entrance of second-stage mill. The second-stage mill and spiral classifier formed a closed system. The spiral classifier separated the coarse grains and then sent them back to entrance of the second-stage mill for milling once again. The fine grain materials past through overflow weir of the spiral classifier and were sent directly to an enriching machine.

(4) After concentrated by the enriching machine, the slurry having high concentration was sent to a ceramic filter for further dewatering, and thus a paste having a water content of 12-35% was obtained, namely the paste is the “female body” of the sialite binary wet cement. Overflow water of the enriching machine together with water from the filter were sent back to the first-stage mill for reutilization.

(5) The “female body” of the sialite binary wet cement was packaged or stored at a storage area for finished bulk product.

2. Flowchart graph for producing the “male body” of the sialite binary wet cement is shown in Figure 6.

(1) Clampshell crane sent the various starting materials batchwisely from the starting material storage areas to hammer crusher for being crushed. The crushed materials were lifted to a distribution belt by a bucket elevator, and were sent to corresponding storehouses for backup.

(2) Storehouses used charge distributors and belt weighers to formulate a mixture in a specific proportion, and a belt conveyer sent the mixture to a mill, and at the same time a given amount of water was supplied continuously to the mill by a pipeline.

(3) The mill and spiral classifier formed a closed system. The spiral classifier separated the coarse grains and then sent them back to entrance of the second-stage mill for milling once again. The fine grain materials past through overflow weir of the spiral classifier and were sent directly to an enriching machine.

(4) After concentrated by the enriching machine, the slurry having high concentration was sent to a ceramic filter for further dewatering, and thus a paste having a water content of 12-35% was obtained, namely the paste is the “male body” of the sialite binary wet cement. Overflow water of the enriching machine together with water from the filter were sent back to the mill for reutilization.

(5) The “male body” of the sialite binary wet cement was packaged or stored at a storage area for finished bulk product.

The present invention is further illustrated by the following examples.

Example 1

Comparison tests between dry-milling and wet-milling of metallurgical slag in A region were taken.

Using same test small mills ($\phi 500*500\text{mm}$), and same milling time, test results were as follows: when dry-milling type was chosen, 5kg starting materials were used, a specific surface area of $3900\text{cm}^2/\text{g}$ was obtained; whereas when wet-milling type was chosen, 7.5 kg starting materials and 3.75 kg water were mixed and grinded, and a specific surface area of $4000\text{cm}^2/\text{g}$ was obtained. It can be seen that, in the case where the materials having approximately same fineness are obtained, wet-milling efficiency is 150% or more of wet-milling efficiency.

Example 2

Comparison tests between dry-milling and wet-milling of the same metallurgical slags as used in Example 1 were taken.

Using same test small mills, and same milling time, when dry-milling type was chosen, 5kg starting materials were used, a specific surface area of $3900\text{cm}^2/\text{g}$ was obtained; whereas when wet-milling type was chosen, 5 kg starting materials and 2.5 kg water were

mixed and grinded, and a specific surface area of $4800\text{cm}^2/\text{g}$ was obtained. It can be seen that, in the case where same milling time is used to mill the materials having same weights, the finesses obtained by the wet-milling is much higher than the finesses obtained by the dry-milling.

Example 3

Cement mortar comparison tests between the sialite binary wet cement of the present invention, and 42.5 grade and 52.5 grade Portland cement were made. In these tests, the following test standards were quoted: *test methods for water requirement for normal consistency, setting time and soundness of the Portland cements* (GB1346-89), *Test method for fineness of cement* (GB1345-91), *Test method for strength of hydraulic cement mortar* (ISO method) (GB/T17671-1999). The testing results are shown in Table 4 and Table 5.

Table 4 physical property of the sialite binary wet cement

Grades	Volume stability	Fineness (%) 0.08mm standard sieve triage	setting time (h:min)	
			initial setting	final setting
42.5 grade Portland cement	acceptable	3.85	3:20	4:55
52.5 grade Portland cement	acceptable	3.5	2:50	4:43
wet cement	acceptable	3.25	3:10	5:50

Table 5 Mechanical property of the sialite binary wet cement

Grades	flexural strength (Mpa)		compression strength (Mpa)	
	3d	28d	3d	28d
42.5 grade Portland cement	4.2	7.1	17.2	45.5
52.5 grade Portland cement	4.5	7.9	24.6	53.9
wet cement	7.8	10.6	32.3	68.9

In the above Table 3 and Table 5, in the wet cement, the “female body” comprises (on dry weight basis) slag 70%, steel slag 10%; and the “male body” comprises (on dry weight basis) anhydrite 14%, lime 6%. The produced “female body” has a specific surface area of $4000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

It can be seen from the data shown in Table 4 and Table 5 for this Example, the sialite binary wet cement of the present invention meets the various national testing standard for

Portland cement, and its intensity index reaches to 62.5 or more MPa.

The following Examples 4-27 described performance index of the mortar obtained by using the sialite binary wet cement of the present invention, stored for different periods under different conditions as a cement material, and adjusting water addition amount so as to have that wet cement (on dry weight basis): standard sand: water = 1: 3: 0.5. In these tests, the following test standards were quoted: *test methods for water requirement for normal consistency, setting time and soundness of the Portland cements* (GB1346-89), *Testing method for specific surface of cement* (Blaine method) (GB8074-87), *Test method for cement strength (ISO method)* (GB/T17671-1999).

The “female body” used in Examples 4-9 is the produced “female body” samples stored for 3 days.

The “female body” used in Examples 10-15 is the produced “female body” samples stored for 3 months.

The “female body” used in Examples 16-21 is the produced “female body” samples stored for 3 days.

Example 4

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 45%, steel slag 28.1%, fly ash 10%, and the “male body” comprises phosphogypsum 9%, lime 6%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 5

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 60%, blast furnace slag 34.8%, borax 0.3%, citric acid 0.1%, and the “male body” comprises phosphogypsum 3%, lime 7%. The produced “female body” has a specific surface area of 4500cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 6

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 55%, phosphate ore slag 12.6%, coal gangue 25%, and the “male body” comprises fluorgypsum 5%, lithium chloride 0.4%, and sodium hydroxide 1.5%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 7

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 45%, titanium slag 16.8%, honey 0.1%, tartaric acid 0.15%, citric acid 0.05%, and the “male body” comprises dihydrate gypsum 20%, chemical industry lime 12%, sulphoaluminate cement 3%, lithium hydroxide 0.4%, sodium carbonate 1%, calcium chloride 1.5%. The produced “female body” has a specific surface area of $4000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 8

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 45%, sugar 0.1%, citric acid 0.2%, borax 0.1%, and the “male body” comprises gypsum 20%, lime 10%, Portland clinker 22.8%, lithium carbonate 0.3%, water glass 1.5%, sodium chloride 1%. The produced “female body” has a specific surface area of $5000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 9

Strength data for the mortar formed by the wet cement are shown in Table 6. In the wet cement (on dry weight basis), the “female body” comprises slag 35%, borax 0.2%, citric acid 0.1%, citric acid 0.1%, and the “male body” comprises phosphogypsum 15%, fluorgypsum 15%, calcium hydroxide 20%, aluminous cement 10.8%, lithium hydroxide 0.3%, sodium carbonate 1.5%, calcium chloride 2%. The produced “female body” has a specific surface area of $5500\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Table 6 Mechanical property of the sialite binary wet cement

No	volume stability	flexural strength (Mpa)		compression strength (Mpa)	
		3d	28d	3d	28d
Example 4	acceptable	6.5	9.2	21.2	57.2
Example 5	acceptable	7.1	9.5	26.9	59.7
Example 6	acceptable	6	9.9	27.1	61.4
Example 7	acceptable	7.5	10.8	36.8	68.2
Example 8	acceptable	7.3	10.6	34.6	66.3
Example 9	acceptable	6.5	9.7	27.6	52.3

Example 10

Strength data for the mortar formed by the wet cement are shown in Table 7. In the

wet cement (on dry weight basis), the “female body” comprises slag 45%, steel slag 30%, fly ash 9.3%, sugars 0.01%, citrate 0.02%, lignosulphonate 0.02%, and the “male body” comprises phosphogypsum 8%, lime 7%, lithium chloride 0.5%, dissolvable carbonate 0.1%, lignosulphonate 0.05%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 11

Strength data for the mortar formed by the wet cement are shown in Table 7, in the wet cement (on dry weight basis), the “female body” comprises slag 60%, zeolite 20.5%, honeys 0.05%, citric acid 0.01%, tartaric acid 0.01%, and the “male body” comprises phosphogypsum 14%, lime 5%, lithium carbonate 0.4%, sodium hydroxide 0.03%. The produced “female body” has a specific surface area of 4500cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 12

Strength data for the mortar formed by the wet cement are shown in Table 7, in the wet cement (on dry weight basis), the “female body” comprises slag 55%, phosphate ore slag 10%, fly ash 9.4%, citric acid 0.03%, boric acid 0.02%, and the “male body” comprises fluorgypsum 6%, lime 14%, Portland cement 5%, lithium hydroxide 0.5%, sugars 0.05%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 13

Strength data for the mortar formed by the wet cement are shown in Table 7, in the wet cement (on dry weight basis), the “female body” comprises slag 50%, titanium slag 16.5%, tartrate 0.03%, lignosulphonate 0.1%, and the “male body” comprises dihydrate gypsum 16%, chemical industry lime 12%, sulphoaluminate cement 5%, lithium carbonate 0.3%, citric acid 0.07%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 14

Strength data for the mortar formed by the wet cement are shown in Table 7, in the wet cement (on dry weight basis), the “female body” comprises slag 45%, lignosulphonate 0.03%, borax 0.17%, and the “male body” comprises gypsum 29.3%, lime 20%, Portland clinker 5%, lithium chloride 0.4%, citric acid 0.1%. The produced “female body” has a specific surface area of 5000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 15

Strength data for the mortar formed by the wet cement are shown in Table 7, in the wet cement (on dry weight basis), the “female body” comprises slag 25%, tartaric acid 0.08%, boric acid 0.02%, and the “male body” comprises phosphogypsum 15%, fluorgypsum 15%, calcium hydroxide 25%, aluminous cement 9.4%, sugars 0.1%, lithium hydroxide 0.4%. The produced “female body” has a specific surface area of 5500cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 7 Mechanical property of the sialite binary wet cement

No.	volume stability	flexural strength (Mpa)		compression strength (Mpa)	
		3d	7d	3d	28d
Example 10	acceptable	8.4	11.5	42.2	78.1
Example 11	acceptable	8	11	38.3	76.5
Example 12	acceptable	8.2	10.7	36.7	72.3
Example 13	acceptable	7.8	10.5	35.6	69.1
Example 14	acceptable	7.5	10.4	34.3	66.9
Example 15	acceptable	4.6	7.9	20.9	43.1

Example 16

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 40%, steel slag 30%, fly ash 13.5%, sugars 0.1%, lignosulphonate 0.25%, and the “male body” comprises phosphogypsum 13%, lime 2%, sodium hydroxide 0.5%, lithium carbonate 0.6%, lignosulphonate 0.05%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 17

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 60%, blast furnace slag 13.8%, honeys 0.15%, tartaric acid 0.15%, and the “male body” comprises phosphogypsum 18%, lime 7%, lithium chloride 0.7%, dissolvable carbonate 0.2%. The produced “female body” has a specific surface area of 4500cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Example 18

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 50%, phosphate ore slag

18.8%, fly ash 5%, citric acid 0.2%, boric acid 0.15%, and the “male body” comprises fluorgypsum 10%, lime 10%, Portland cement 5%, sugars 0.15%. The produced “female body” has a specific surface area of $4000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 19

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 50%, titanium slag 14%, tartrate 0.2%, lignosulphonate 0.2%, and the “male body” comprises dihydrate gypsum 20%, chemical industry lime 12%, sulphaaluminate cement 3%, lithium hydroxide 0.5%, honeys 0.1%. The produced “female body” has a specific surface area of $4000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 20

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 44.1%, lignosulphonate 0.3%, borax 0.2%, and the “male body” comprises gypsum 35%, lime 15%, Portland clinker 4.8%, lithium hydroxide 0.5%, tartaric acid 0.1%. The produced “female body” has a specific surface area of $5000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 21

Strength data for the mortar formed by the wet cement are shown in Table 8. In the wet cement (on dry weight basis), the “female body” comprises slag 35%, lignosulphonate 0.1%, tartaric acid 0.1%, boric acid 0.02%, and the “male body” comprises phosphogypsum 10%, fluorgypsum 20%, calcium hydroxide 20%, aluminous cement 15%, lithium chloride 0.6%, citric acid 0.18%. The produced “female body” has a specific surface area of $5500\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Table 8 Mechanical property of the sialite binary wet cement

No.	volume stability	flexural strength (Mpa)		compression strength (Mpa)	
		3d	7d	3d	28d
Example 16	acceptable	8.1	10.9	39.6	77.2
Example 17	acceptable	7.6	11.2	36.5	75.7
Example 18	acceptable	8.1	11.5	36.8	71.4
Example 19	acceptable	7.3	10.6	35.9	68.2
Example 20	acceptable	7.5	10.3	33.7	66.3

Example 21	acceptable	6.2	9.5	26.4	52.3
Example 22	acceptable	8.2	10	46.8	74.8

The following is to describe the working examples having different starting materials and different proportioning for obtaining the mortars.

Example 22

Strength data for the mortar formed by the wet cement are shown in Table 9. In the wet cement (on dry weight basis), the “female body” comprises slag 49.15%, steel slag 40%, tartaric acid 0.3%, boric acid 0.05%, and the “male body” comprises lithium carbonate 0.5%, water glass 10%. The produced “female body” has a specific surface area of $4500\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 23

Strength data for the mortar formed by the wet cement are shown in Table 9. In the wet cement (on dry weight basis), the “female body” comprises burned coal gangue 80%, lignosulphonate 0.1%, tartaric acid 0.1%, and the “male body” comprises water glass 18%, lithium chloride 0.3%, sodium chloride 1.5%. The produced “female body” has a specific surface area of $5000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 24

Strength data for the mortar formed by the wet cement are shown in Table 9. In the wet cement (on dry weight basis), the “female body” comprises crushed brick 78%, citric acid 0.2%, and the “male body” comprises water glass 20%, lithium hydroxide 0.3%, and sodium chloride 1.5%. The produced “female body” has a specific surface area of $5000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Example 25

Strength data for the mortar formed by the wet cement are shown in Table 9. In the wet cement (on dry weight basis), the “female body” comprises phosphate ore slag 97%, and the “male body” comprises lime 2.7%, lithium hydroxide 0.3%. The produced “female body” has a specific surface area of $5000\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Table 9 Mechanical property of the sialite binary wet cement

No.	volume stability	flexural strength (Mpa)	compression strength (Mpa)
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		3d	7d	3d	28d
Example 22	acceptable	8.2	10	46.8	74.8
Example 23	acceptable	3.8	5.9	15.6	39.2
Example 24	acceptable	3.1	5.9	11.6	23.2
Example 25	acceptable	4.1	6.3	14.9	31.5

Example 26

Strength data for the mortar formed by the wet cement are shown in Table 10. In the wet cement (on dry weight basis), the “female body” comprises Sample 1, Sample 2, Sample 3 shown in Table 2 with a content of 75% respectively, and citric acid 0.2%, and the “male body” comprises gypsum 15%, lime 8%, lithium hydroxide 0.3%, sodium chloride 1.2%, calcium chloride 0.5%. The produced “female body” has a specific surface area of 5000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 10 Mechanical property of the sialite binary wet cement

Sample No.	initial setting hour: min	final setting hour: min	stability	flexural strength (MPa)		compression strength (MPa)	
				3 days	28 days	3 days	28 days
Sample 1	2: 20	3: 45	acceptable	8.1	10.2	31.2	57.2
Sample 2	2: 10	3: 25	acceptable	7.3	11.3	35.2	69.8
Sample 3	2: 45	5: 50	acceptable	6.9	10.5	26.7	63.9

Example 27

Strength data for the mortar formed by the wet cement are shown in Table 11. In the wet cement (on dry weight basis), the “female body” comprises sample 4, sample 5, sample 6 shown in Table 3 with a content of 75% respectively, and citric acid 0.2%, and the “male body” comprises gypsum 15%, lime 8%, lithium hydroxide 0.3%, sodium chloride 1.2%, calcium chloride 0.5%. The produced “female body” has a specific surface area of 5000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 11 Mechanical property of the sialite binary wet cement

Sample No.	initial setting hour: min	final setting hour: min	stability	flexural strength (MPa)		compression strength (MPa)	
				3 days	28 days	3 days	28 days
Sample 4	2: 35	3: 50	acceptable	8.45	10.4	32.5	56.2
Sample 5	2: 5	3: 30	acceptable	7.5	11.1	36.4	70.6
Sample 6	2: 40	5: 45	acceptable	7.2	10.3	27.5	62.5

The following is to describe the situation where the sialite binary wet cement is used for mining backfill.

Example 28

In the following Table 12 is shown river sand strength for mining backfill when using the sialite binary wet cement consolidates the river sand.

In the wet cement (on dry weight basis), the “female body” comprises slag 65%, blast furnace slag 13.7%, lignosulphonate 0.1%, and the “male body” comprises phosphogypsum 9%, lime 11%, sodium hydroxide 0.8%, lithium carbonate 0.4%. The produced “female body” has a specific surface area of $4500\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Table 12 Strength of river sand consolidated by using the sialite binary wet cement

No.	Soil content in sand (%)	wet cement %	Concentration %	Compression strength (Mpa)				
				1 day	3 days	7 days	28 days	60 days
1	10	3	80	0.41	0.54	0.73	1.8	2.1
2	15	3	80	0.45	0.61	0.9	2	2.4
3	20	3	80	0.48	0.65	0.96	2.2	2.45
4	25	3	80	0.51	0.68	1.2	2.4	2.5
5	30	3	80	0.6	0.7	1.4	2.6	2.8
6	40	3	80	0.59	0.71	1.45	2.6	2.78

Example 29

In the following Table 13 is shown mine tailings strength for mining backfill when the mine tailings is consolidated by using the sialite binary wet cement.

In the wet cement (on dry weight basis), the “female body” comprises slag 71.4%, blast furnace slag 10%, citric acid 0.1%, boric acid 0.15%, and the “male body” comprises fluorgypsum 10%, lime 8%, lithium chloride 0.3%, citric acid 0.05%. The produced “female body” has a specific surface area of $4500\text{cm}^2/\text{g}$, and the produced “male body” has a specific surface area of $4000\text{cm}^2/\text{g}$.

Table 13 Strength of mine tailings consolidated by using the sialite binary wet cement

No.	Tailings content %	wet cement %	Concentration %	compression strength (Mpa)				
				1 day	3 days	7 days	28 days	60 days
1	69	3	72	0.3	0.42	0.5	1.2	1.4
2	72	3	75	0.38	0.46	0.54	1.42	1.78

The following is to describe a method for producing building block by using the sialite binary wet cement.

Example 30

Strength data of fly ash consolidated by using the sialite binary wet cement are shown in the following Table 14. A part of the wet cement (on dry weight basis) was homogeneously mixed with fly ash in a ratio of 1: 9, water was homogeneously mixed with the other part of the wet cement (on dry weight basis) in a ratio of 0.2: 1, and then they were incorporated into a mold, and were subjected to jolt moulding and then curing in standard curing case. Flexural strength and compression strength of the concrete were measured respectively after being cured for 3 days, 7 days and 28 days. In the wet cement (on dry weight basis), the “female body” comprises slag 45%, steel slag 35%, lignosulphonate 0.3%, borax 0.2%, and the “male body” comprises phosphogypsum 6%, lime 12%, sodium hydroxide 1%, lithium hydroxide 0.4%, tartaric acid 0.1%; The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 14 Strength of fly ash consolidated by using the sialite binary wet cement

No.	flexural strength (Mpa)			compression strength (Mpa)		
	3d	7d	28d	3d	7d	28d
1	1.8	2.9	3.5	4.2	8.5	11.5
2	2.1	3.2	3.8	5	9.4	15

Example 31

Strength data of fly ash consolidated by using the sialite binary wet cement are shown in the following Table 15. A part of the wet cement (on dry weight basis) was homogeneously mixed with fly ash in a ratio of 1: 5, water was homogeneously mixed with the other part of the wet cement (on dry weight basis) in a ratio of 0.2: 1, and then they were incorporated into a mold, and were subjected to jolt moulding and then curing in standard curing case. Flexural strength and compression strength of the concrete were measured respectively after being cured for 3 days, 7 days and 28 days. In the wet cement (on dry weight basis), the “female body” comprises slag 50%, phosphate ore slag 26.9%, sugar 0.1%, citric acid 0.2%, and the “male body” comprises phosphogypsum 6%, lime 13%, sodium carbonate 1%, lithium carbonate 0.3%, water glass 1.5%, sodium chloride 1%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 15 Strength of fly ash consolidated by using the sialite binary wet cement

No.	flexural strength (Mpa)	compression strength (Mpa)
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	3d	7d	28d	3d	7d	28d
1	3	4.9	5.2	11.1	15.3	20.6
2	3.2	5.1	5.4	11.5	16	22

Example 32

Strength data of fly ash consolidated by using the sialite binary wet cement are shown in the following Table 16. The wet cement (on dry weight basis) was homogeneously mixed with sand soil, and then they were incorporated into a mold, and were subjected to jolt moulding and then curing in standard curing case (20°C). Flexural strength and compression strength of the concrete were measured respectively after being cured for 3 days, 7 days and 28 days. In the wet cement (on dry weight basis), the “female body” comprises slag 60%, steel slag 16.85%, honey 0.15%, tartaric acid 0.1%, and the “male body” comprises fluorgypsum 8%, lime 11%, lithium hydroxide 0.4%, sodium carbonate 1%, calcium chloride 1.5%, water glass 1%. The produced “female body” has a specific surface area of 4000cm²/g, and the produced “male body” has a specific surface area of 4000cm²/g.

Table 16 Strength of clay consolidated by using the sialite binary wet cement

No.	soil content in sand (%)	wet cement %	Water content %	compression strength (Mpa)			flexural strength (Mpa)		
				3d	7d	28d	3d	7d	28d
1	2	10	10	6.9	12	17	1.8	2.9	3.7
2	30	10	10	10	15	20	2.3	3	4
3	50	10	11	11	16	25	2.4	3.2	4.2
4	80	10	15	7	13	16	2	3	3.8

It can be seen from the above experiments and tests that, the sialite binary wet cement of the present invention is able to substitute the traditional cements for using in building, but also is a good backfill and timbering material, and it can be used for mining backfill and timbering materials, and subgrade strengthening materials, and it has very strong consolidation capacity, especially for sand soil having a high clay content.